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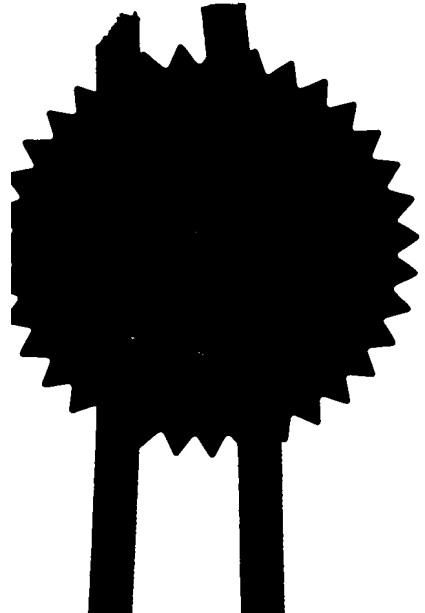
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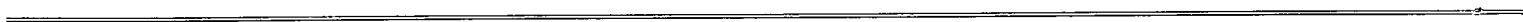
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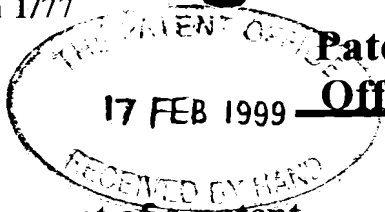


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4. Title of the invention

A MEASUREMENT METHOD AND MEASUREMENT APPARATUS

5. Name of your agent (if you have one)

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Claim(s) 7 *81*

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*Boult Wade Tennant*

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**Dr.R.G.Jenkins**  
**0171 404 5921**

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A MEASUREMENT METHOD AND MEASUREMENT APPARATUS

The present invention relates to a measurement method and measurement apparatus employing an  
5 interferometer arranged to form patterns of interference fringes.

Interferometers are well-known, and the testing and measurement of optical components, from simple spectacle lenses to astronomical telescopes requires  
10 an interferometer system of one sort or another. Interferometers are also now routinely applied in engineering for the measurement of mechanical and thermal behaviour of materials and components.

Conventionally, for the most accurate measurement  
15 these interferometer systems are constructed from high-quality optical elements and include fine controls for precise alignment. The need for high quality, precise components makes interferometer systems expensive and places practical restrictions on  
20 the aperture of the instrument. Typically, the controls are adjusted to reduce the number of interference fringes formed in the observer's field of view before the test or measurement is performed to a minimum, and ideally zero. Then, an object to be  
25 tested is inserted in one arm of the interferometer, or the interferometer is perturbed (altered) in some other way. If the interferometer was initially set up to produce a fringe-free field, then all interference fringes appearing in the test interferogram are due to  
30 the perturbation.

In conventional interferometer measurement applications, a few fringes in the initial (i.e. reference) interferogram may be tolerated, if the test/measurement perturbation results in an  
35 interference pattern having a large number of fringes.

The underlying imperfections in the unperturbed interferometer may be ignored.

~~If, however, the test/measurement perturbation~~  
itself only introduces a small number of fringes,  
5 then the underlying imperfections cannot simply be ignored.

Techniques are known for removing the effects of aberrations in the reference interferogram so as to display an image from a test component which is free  
10 from spurious fringes generated by an imperfect optical system. The method for applying the correction is, however, both elaborate and slow. From one or more interferograms of the reference and test object the phase distributions are calculated. The  
15 method typically necessitates the conversion of at least three test interference fringe patterns (interferograms) and at least three reference interferograms into digital images to facilitate processing. The three or more reference and test  
20 interferograms are phase stepped (shifted) from each other by pre-determined amounts. These phase shifted patterns are generated sequentially by the appropriate phase shifting of fringes, for example by a piezoelectric transducer (PZT)-driven mirror or  
25 wavelength modulation.

Once the phase distributions (phase maps) have been calculated an unwrapping procedure is then applied to the phase maps. As the test phase maps also contain the reference information, subtraction of the  
30 reference map from the test map results in the presentation of the test information only. As a consequence of the delay, the subtraction is usually performed off-line and post-operatively. In addition, the approach may fail because the phase calculation  
35 and unwrapping procedures will not tolerate

interferograms with excessive numbers of closely spaced fringes or fringes which are contorted.

It is also known to derive an accurate phase map of the optical path perturbation resulting from a test component by deliberately introducing carrier fringes (a spatial carrier) into the test interferogram by, for example, tilting a mirror in the interferometer, and performing a Fourier transform analysis method. Rather than requiring at least three reference interferograms, with the Fourier transform method only one fringe pattern having a spatial carrier is enough for the analysis. However, it requires more computation for Fourier transformation and filtering and cannot be conducted in real-time. Therefore it has not been easy to accelerate fringe analysis for quick applications such as feedback control of optical instruments and real-time monitoring of dynamic phenomena.

The paper "Video-rate fringe analyzer based on phase-shifting electronic moiré patterns", Kato et al, Applied Optics, 10 November 1997, Vol. 36, No. 32, p8403 - describes a fringe analyzer that delivers the phase distribution at a video-rate from a fringe pattern containing a spatial carrier. It is based on parallel generations of three phase-shifted moiré patterns through electronic multiplication with computer-generated reference gratings and low-pass filtering. The phase distribution is derived by the subsequent parallel processing of these patterns on the basis of a three-step phase-shifting algorithm.

Image processing involving digital subtraction of images is known in digital speckle pattern interferometry (described, for example, in "Speckle Metrology", Ed. R.S. Sirohi, Marcel Dekker, Inc. New York, 1993, p125) and in document analysis (described,

for example, in "A new method for displaying indented and other markings on documents", C. Forno, Science and Justice 1995, 35(1) 45-51).

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5 Moiré fringe generation is a known process  
whereby the intensity distributions of two dissimilar  
grid patterns are combined, for example by  
superimposition, as described in Chapter 6, "Handbook  
of Experimental Mechanics", Society for Experimental  
Mechanics Inc, Prentice Hall, Englewood Cliffs, New  
10 Jersey 07632, USA 1987, ISBN:0-3-377706-5. By  
superimposing the dissimilar grids, a moiré fringe  
pattern is generated which represents the local  
differences between the spatial frequencies of the  
grids.

15 According to a first aspect of the present  
invention, there is provided a measurement method  
comprising the steps of:

arranging an interferometer to form a first  
interference fringe pattern comprising at least ten  
20 interference fringes;

recording an image of said first interference  
fringe pattern;

25 perturbing an optical path in the interferometer  
to form a second interference fringe pattern  
comprising at least ten interference fringes; and

combining an image of said second interference  
fringe pattern with the recorded image of the first  
interference fringe pattern to produce a further image  
comprising a moiré fringe pattern arising from a  
30 difference or differences between the first and second  
interference fringe patterns.

Thus, it is no longer necessary to align the  
interferometer with great precision to produce a  
substantially fringe free reference (i.e. first)  
35 interference fringe pattern before the test or



measurement is performed (i.e. before the interferometer is perturbed/alterd).

5 The moiré fringe pattern produced by combining the first and second interference fringe patterns is determined by the perturbation itself, and not by the underlying imperfections and misalignments of the unperturbed interferometer.

10 In this new approach, all the errors of a poor quality, misaligned system are accepted and then eliminated by the combination process, producing a moiré fringe pattern. The method enables very large aperture optical systems for traditional and engineering interferometers to be constructed from inexpensive and basic components.

15 A conventional high quality optical measurement interferometer will typically comprise optical components having surfaces manufactured to tolerances of better than  $\lambda/10$  or even  $\lambda/100$  where  $\lambda$  is the wavelength of light input to the interferometer.

20 With the inventive method, imperfections in optical components as large as  $100\lambda$  or greater may be tolerated.

25 The interferometer used in the present invention may be an optical interferometer, or alternatively may be an interferometer arranged to form an interference pattern from incident electromagnetic radiation having different wavelength.

30 In a basic form, the method may be implemented by recording the first image on, for example, a photographic film. The subsequent interference fringe pattern, produced by perturbing the interferometer system, may then be projected onto the recorded image and the resultant moiré fringe pattern observed.

35 Alternatively, the recorded image may be captured by a camera, such as a high resolution electronic

camera where the image of the interference pattern is focused onto a CCD (Charge Coupled Device) sensing element.

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5       The images combined to produce the moiré fringe pattern may be digital images, facilitating the processing and enabling a variety of combination procedures to be employed, for example subtraction, multiplication, addition, and/or superimposition.

10       Thus, the combining step may comprise one or more of the steps of adding, subtracting, filtering, superimposing, or multiplying the images.

Advantageously the images of the first and second interference fringe patterns may be combined by a process of digital subtraction.

15       In order to produce moiré fringe patterns, each of the first and second interference fringe patterns clearly needs to comprise a number of fringes. Ten is a practical lower limit, but better. (i.e. more detailed) moiré fringe patterns may be obtained by  
20       increasing the number of fringes in the first and second patterns.

Advantageously, the method may therefore include the step of tilting a reflecting surface of the interferometer to increase the number of interference  
25       fringes.

30       If the components of the interferometer are sufficiently irregular, or the alignment is already sufficiently poor, however, then no further adjustment may be needed to provide an interference fringe pattern comprising a large number of fringes.

Advantageously, the first interference fringe pattern may comprise at least fifty, and preferably at least 100 fringes.

35       Preferably, the spatial frequency of the fringes in the first (reference) interference pattern should

be higher than the spatial frequency of fringes that would be introduced by the measurement/test perturbation, were the interferometer set up to

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5 produce an initial fringe-free field, i.e. the carrier fringe spatial frequency should be higher than the spatial frequency of the phase distribution to be measured.

10 The number of fringes in the first interference fringe pattern may be larger than, smaller-than, or the same as the number in the second pattern.

15 The perturbation may result in the second interference fringe pattern having fewer fringes than the first pattern, but ideally the interferometer should be arranged so that the number of fringes in the interference fringe pattern produced by the interferometer is increased by the perturbation, i.e. the second pattern comprises more fringes than the first. For example, a detailed moiré fringe pattern may be produced by combining a first image of 100  
20 fringes with a second image of 150 fringes.

The perturbation to the interferometer system may take a number of forms. For example, the step of perturbing may comprise the step of inserting a transparent test object in the optical path (e.g. inserting the object in one arm of the  
25 interferometer).

The step of perturbing may comprise the distortion, rotation, and/or translation of a reflecting surface or a transparent object in the  
30 optical path.

The step of perturbing may comprise the step of replacing a reference object with a test object, and the first interference fringe pattern may have been recorded with the reference object in place.

35 The step of perturbing may alternatively, or in

addition, comprise the step of disturbing a gas and/or disturbing the flow of a gas in the optical path.

The image of the second interference fringe

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5 pattern may also be a recorded image, or alternatively may be a live image output by a camera.

Advantageously one or both of the recorded image of the first interference fringe pattern and the image of the second interference fringe pattern may be images selected from a recorded sequence of images of  
10 the interference fringe pattern formed by the interferometer.

Advantageously the recorded image of the first interference fringe pattern and the image of the second interference fringe pattern may be digital  
15 images.

Preferably, the step of combining includes the step of subtracting one of the digital images from the other. Advantageously, with modern image processing software, the subtraction computation is trivial and  
20 can be performed, and the result (the further image) displayed almost continuously in real time.

Thus, by applying the principles of moiré in digital form to interferometry, optical aberrations can be made inconspicuous and apart from the time  
25 required to perform a simple image subtraction between reference and object images, there are no other delays in presenting the corrected interferogram. In addition, the method can better accommodate gross aberrations, thus offering the opportunity of  
30 constructing systems from inexpensive components of poor optical quality. There is no need to align the interferometer precisely and so an economy can be made on the quality of the mechanical adjustments.

Advantageously, the step of combining may include the  
35 step of converting negative values obtained in the

subtraction process to positive values. Thus, the image resulting from the subtraction may be rectified, which provides the advantage that the frequency of the

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5     rectified pattern is double that of the carrier (i.e. the spatial frequency of the first interference fringe pattern). This property improves the discrimination of the moiré fringe pattern over the carrier compared with alternative processing techniques, such as addition where the carrier frequency is preserved. The  
10    further image will, of course, in general include the moiré fringe pattern and a finer pattern at, or close to, the carrier frequency.

      The method may further comprise the steps of arranging the interferometer to form a third  
15    interference fringe pattern;

      recording an image of the third interference fringe pattern;

      arranging the interferometer to form a fourth interference fringe pattern;

20    recording an image of the fourth interference fringe pattern, wherein the first, third and fourth interference fringe patterns are phase shifted from each other by predetermined amounts; and

      combining the image of the second interference  
25    fringe pattern with each of the recorded images of the first, third and fourth interference fringe patterns to produce respective said further images; and

      processing the further images to produce a phase map of the perturbation of the optical path.

30    Thus, at least three phase-stepped "reference" interferograms may be generated and recorded, and combined with the second interference fringe pattern, i.e. the test interferogram, to produce respective further images.

35    The phase shifting or stepping may be achieved by

conventional means (for example the use of piezoelectric transducer-driven mirrors).

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~~Advantageously, the image of the second (test)~~

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5 interference fringe pattern may be an image selected from a recorded sequence of images of the interference pattern formed by the interferometer.

Thus, the changing interference pattern during a test may be recorded in real time, and then analysed at a later time by processing with the at least three  
10 phase stepped reference images to produce a full phase map of the perturbation at any given time in the measurement process.

Advantageously, the images of both the first and second patterns may be images selected from a recorded  
15 sequence of images of the interference pattern formed by the interferometer. Thus, the resultant moiré fringe pattern in the further image is indicative of only the changes in the interferometer arrangement between the two selected times.

20 Any two images (i.e. interferograms) may be selected from a recorded sequence and combined (e.g. digitally processed) to produce a resultant image comprising a moiré fringe pattern indicative of the change to the interferometer between the times at  
25 which the selected images were recorded.

Images of the interference fringe patterns formed by the interferometer may be captured and output as a continuous stream or sequence from an electronic camera. Each image may be combined with the stored  
30 first image to produce a respective further image and respective moiré fringe pattern which may be displayed in real time, e.g. at video rate.

According to a second aspect of the present invention there is provided measurement apparatus  
35 comprising:

an interferometer arranged to form interference fringe patterns comprising at least ten interference fringes;

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5 a camera arranged to capture images of the interference fringe patterns;

an image store arranged to store an image of the interference fringe pattern captured by the camera at a selected time;

10 an image processor arranged to combine the stored image with an image of the interference fringe pattern captured by the camera at a different time to produce a further image comprising a moiré fringe pattern arising from a difference or differences between the interference fringe patterns at the selected and said  
15 different time.

The interferometer may be arranged to form interference fringe patterns comprising at least fifty interference fringes, and the images may be digital images.

20 The image processor may be arranged to produce the further image by a process including at least the subtraction of one of the digital images from the other.

Additional processing may be performed on the  
25 images, such as filtering or normalisation of intensity distributions. This further processing may be performed on the images before, during, or after their combination to produce the further image including a moiré fringe pattern.

30 The further image or images may also be processed, for example by filtering to remove the underlying carrier fringe pattern and so leave only the moiré fringe pattern.

The image processor may be arranged to produce  
35 the further image by a process including the

conversion of negative values obtained in the subtraction process to positive values, i.e. the processor may be arranged to rectify the intensity distribution calculated by subtraction.

5           The interferometer may include means for phase shifting the interference fringe patterns by predetermined amounts, the image store may be arranged to store images of the interference fringe patterns captured by the camera at at least three different  
10           selected times, the image processor may be arranged to combine each stored image with the image captured at a different time to produce a respective further image comprising a respective moiré fringe pattern, and the image processor may be further arranged to process the  
15           further images to produce a phase map. This phase map may be indicative of the perturbation to the interferometer between the different time and the time of capture of one of the stored images.

          The camera may be arranged to output a continuous  
20           sequence of captured images of the interference fringe pattern, and the image processor may be arranged to combine the or one of the stored images with each one of the sequence of captured images and to produce a respective further image, which may be stored. The  
25           apparatus may further comprise a display for displaying the sequence of further images, and each further image may be displayed substantially as soon as it is produced. The sequence of further images may be displayed and/or stored at the same rate as the  
30           capture of images by the camera.

          The measurement apparatus may further comprise an image recorder for recording the images captured by the camera, and an image selector for selecting one of the recorded images to be used as the stored image or  
35           the image to be combined with the stored image.



Alternatively, both images may have been selected from a sequence of recorded images.

The camera may be a CCD camera to provide high resolution and fast response.

5            Advantageously, the interferometer may have an aperture of at least 10cm. The aperture may be as large as 1m, or larger still, as the further image production process inherently rejects the underlying imperfections in the interferometer components.

10           The advantage of subtracting one image from another (i.e. subtracting one intensity distribution from another) is that wherever the images are the same (the intensities are the same) the resultant image  
15 will show a dark region.

            Generally, increasing the number of fringes in the first interference fringe pattern (i.e. the reference interferogram) increases the detail on the resultant moiré fringe pattern and improves the  
20 resolution of the perturbation to the interferometer. However, an upper limit to the density of the fringes (i.e. the maximum spatial frequency of the fringes in the recorded image of either the first interference  
25 fringe pattern or the second (test) pattern) is set by the resolution of the means used to record the image, for example the resolution or pixel density of the camera used to capture the image and the capacity of the image store used to hold the recorded image.

            Embodiments of the present invention will now be  
30 described with reference to the accompanying drawings in which:

            Fig. 1 is a schematic diagram of measurement apparatus in accordance with an embodiment of the present invention, incorporating a Michelson  
35 interferometer;

Fig. 2a is an image of an interference fringe pattern (interferogram) formed using the measurement apparatus of Fig. 1;

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5 Fig. 2b is a representation of a further image obtained using the apparatus of Fig. 1, comprising a pattern of moiré fringes;

Fig. 3a is a digitally subtracted moiré interferogram of gas emerging from a butane lighter obtained using apparatus similar to the embodiment  
10 shown in Fig. 1;

Fig. 3b is a digitally subtracted moiré interferogram of a gas flame, obtained using apparatus in accordance with the embodiment shown in Fig. 1;

Fig. 4a is a DMS interferogram produced from grating interferometry applied to a notched  
15 specimen, with a small deformation added to a highly deformed state (one fringe = 0.42 microns x-displacement);

Fig. 4b is a sheared DMS image of the specimen in  
20 Fig. 4a, showing strain contours at approximately 0.05% intervals;

Fig. 5 is a schematic diagram of a large aperture interferometer using simple uncoated optical components, suitable for use with methods embodying  
25 the present invention;

Fig. 6a shows a DMS interferogram from the Fresnel lens interferometer of Fig. 5 with a tilt of plate P2;

Fig. 6b shows a DMS interferogram from the  
30 Fresnel lens interferometer of Fig. 5 of hot air flow above a soldering iron;

Fig. 7 shows an interference fringe pattern derived from a grating interferometer with a well-corrected collimating lens;

35 Fig. 8 is an interference fringe pattern showing

the effect of introducing a poor quality optical component into the grating interferometer used to produce the pattern of Fig. 7; and

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Fig. 9 is an x-strain contour map of a sheared  
5 and digitally subtracted grating interferometry image produced using a method in accordance with an embodiment of the present invention.

A method in accordance with a preferred  
embodiment of the present invention includes a process  
10 which shall be referred to as Digital moire subtraction (DMS). The interferometer is configured with a means of introducing carrier, or tilt fringes in the interferogram, with the number of fringes across the field variable, but within the resolution  
15 of the image camera and frame store. This can usually be accomplished by manual adjustment of a mirror. The image is captured, digitally stored and used as a reference. Subsequently acquired images are then subtracted from the reference and the difference  
20 displayed.

Both reference and all subsequent images consist of fine, quasi-regular fringe patterns, which are equally distorted by the combined optical aberrations of all the interferometer components. If the patterns  
25 are identical, when the two digitised intensity distributions are subtracted the result is a dark, fringe-free field. If one image is modified by changes in the optical path length of one arm of the interferometer, caused by formation of a test  
30 component, perturbations or other optical effects, fringes are generated which represent the changes only. Detailed analysis of the fringe pattern can be carried out directly on the moiré interferogram, for example by phase stepping, phase unwrapping and  
35 differentiation. One important feature of this

analysis is that it operates on a single interferogram of the test field.

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~~In the process of subtracting the spatial carrier~~

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5 patterns of two interferograms with a small shift in  
phase between them, the resulting absolute values of  
intensity will oscillate about zero. When rectified  
the frequency of the pattern is double that of the  
carrier. This property improves the discrimination of  
the moiré fringe pattern over the carrier compared  
10 with alternative processing techniques, such as  
addition where the carrier frequency is preserved.

An on-line image subtraction facility is a  
standard feature of most image processing software.  
Since the subtraction computation is trivial, it can  
15 be performed and the result displayed almost  
continuously in real-time.

The DMS approach has been assessed on a number of  
optical systems with a view to demonstrating its  
potential. Applying embodiments of the inventive  
20 method to conventional Michelson interferometry (see  
e.g. Born M. and Wolf E., Principles of Optics,  
Pergamon Press, Oxford, 6th ed., 300-302) and its  
derivatives, the advantage of using low-quality  
components and imprecise adjustment controls are  
25 clear. These benefits can be exploited in grating  
interferometry (see e.g. Post D., et. Al., High  
sensitivity moiré, experimental analysis for mechanics  
and materials, Springer Verlag, New York (1994) and,  
in addition there are other features which enhance the  
30 range of measurements.

Measurement apparatus in accordance with an  
embodiment of the present invention, incorporating a  
Michelson interferometer 1 is shown in schematic form  
in Figure 1. With an aperture of 60mm square, it  
35 comprises: 2 plano-convex borosilicate crown glass

lenses (L1, L2), one semi-transparent beam splitter (BS) and 2 fully reflecting mirrors (M1, M2). The mirrors are front-surfaced, but coated on standard

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5 produced by front and rear surface reflections from the beam splitter have been eliminated by converting it into a small angle hollow prism, with a sheet of uncoated glass for the opposite window and with the prism filled with liquid paraffin.

10 Illumination is provided by a He-Ne laser, 9 fitted with a diverging objective at a distance approximating to the focal length of the interferometer collimating lens (L1). The second lens, at the exit of the system acts as a field lens  
15 for the CCD camera used to capture and record the interferograms. The apparatus is arranged such that the patterns of interference fringes produced by the interferometer 1 are focussed onto the CCD sensing element of the camera. The camera outputs a  
20 continuous stream of captured digital images  $I(t)$  and an image store 3 is arranged to record an image captured at a selected time. The apparatus includes an image recorder arranged to record the sequence of captured images, which can also play the images back  
25 to the image processor 4. The image processor 4 combines the stored image  $I(t_1)$  with the live image or image retrieved from the recorder 7 to produce a further image FI including a moiré fringe pattern. The further images are displayed on a display 5 in real  
30 time (at video rate) and/or may be recorded by the, or another, recorder 6. Briefly, the mechanism for generating interference fringes is by interference between the two reflected beams from M1 and M2, which are added at BS. Any perturbation of one beam  
35 resulting from the insertion of an optical component,

or refractive index variation caused, for example by convective flow, will disturb the wavefront of this beam and produce interference fringes.

Figure 2(a) shows the distribution of interference fringes 11 generated solely by the combined errors in the optical components of the interferometer. There are so many fringes present that it is not possible to optimise the alignment of the system. Moreover, the fringes are so closely spaced and contorted as to prevent the application of automatic fringe analysis methods. It would not be unreasonable to consider that an interferometer possessing such gross aberrations would be of little or no use as a measurement instrument.

A tilt was applied to one mirror in order to produce an even finer pattern, largely free from broadly spaced fringes. In a method embodying the present invention, this image is captured and then digitally subtracted from the live image. The optical errors in the interferometer are thus removed making it is sensitive only to the errors of the introduced test component. As a test, by introducing an additional small tilt (i.e. a tilt in addition to the tilt applied to produce the even finer pattern) to one mirror the subtracted moiré interferogram of Figure 2(b) was produced. Such straight and uniformly spaced moiré fringes 12 are normally expected only from an interferometer possessing a high degree of optical correction.

There is a slight curvature to the moiré fringes at the edges of the field which is due to the geometric distortion introduced by the CCD camera lens and L2. This can be compensated optically by choosing a lens combination that is better corrected, or mathematically by reference to a look-up table of the

field distortion.

Figure 3(a) demonstrates an application of DMS to display the induced refractive index distribution of

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unlit gas emerging from a butane lighter and Figure  
5 3(b) the interferogram produced when the gas is  
ignited. Without digital moiré subtraction, the subtle  
influences of the gas and flame would have been  
inconspicuous when superimposed on the untreated  
interferogram. The inventive method may be used on a  
10 Mach-Zehnder interferometer system (see e.g. Born  
M. and Wolf E., Principles of Optics, Pergamon Press,  
Oxford, 6th ed., 312-314) in the field of convective  
flow.

The moiré interferograms of figs 3(a) & 3(b) each  
15 comprise a pattern of moiré fringes 12 visible over  
the carrier interference fringes (at higher spatial  
frequency). The moiré fringes are not formed by the  
interferometer, but instead by the combination of  
direct interference fringe patterns formed by the  
20 interferometer 1.

Embodiments of the present invention are suitable  
for the measurement of optical flatness and lens  
aberrations.

The digital moiré approach has potential  
25 application in the design of large aperture  
interferometers. In a Fizeau system (see e.g. Born M.  
and Wolf E., Principles of Optics, Pergamon Press,  
Oxford, 6th ed., 286-291), for measuring optically  
flat surfaces, the main component is a stable, high  
30 quality reference flat from which a second surface can  
be compared. Providing the long-term stability of the  
optical arrangement is preserved, DMS offers a way of  
relaxing the tolerances on the surface figure of the  
flat as well as the auxiliary components, including  
35 the beam splitting element.

In an embodiment of the inventive method, a non-optimised Fizeau interferometer is initially calibrated using a master flat in the measurement

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5     interferogram which is then captured and stored.  
Without further adjustment, the master is removed and replaced with the test component. The master flat image is subtracted and the result (i.e the further image comprising moiré fringes) represents height  
10    contours of the component's surface.

      In this way, there is no requirement to keep a high quality reference surface in the system, instead, the initial reference interferogram can be stored permanently. However, if there are doubts about the  
15    stability of the interferometer, then it may be advisable to refresh the master flat moiré interferogram by repeating the calibration from time to time. It is possible to envisage that a single master flat could be used as an International Standard  
20    in the setting up of individual local Fizeau systems.

      For the measurement of lens aberrations, a Twyman-Green system (see e.g. Born M. and Wolf E., Principles of Optics, Pergamon Press, Oxford, 6th ed., 302-305) is appropriate. The symmetric and asymmetric  
25    aberration terms can be displayed in the resulting interferogram by respectively translating and rotating the lens in the interferometer.

      A similar approach to the Fizeau method can be applied in lens testing, where the master fringe  
30    interferogram of a well-corrected lens is stored permanently and compared with the test lens.

      Embodiments of the inventive method are employed in moiré or grating interferometry.

      This sensitive and versatile in-plane deformation  
35    measurement technique is based in its simplest form on



a mirror system which is illuminated with an expanded and collimated laser beam. A well-corrected, achromatic lens is usually employed in collimation

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because of its minimal spherical aberration and the consequent reduction in the number of initial reference fringes. In one system, containing an expensive, high quality collimating lens and a nominally perfect specimen grating, the residual fringe pattern represents a potential uncertainty, unless compensated, of 25 microstrain and in most applications this would be considered negligible and ignored. Such an "ideal" unperturbed interference fringe pattern is shown in fig 7.

To test the DMS approach on compensating for aberrations in grating interferometry, rather than dismantle the system and install inferior components, a defective optical element was introduced into the system so as to effectively degrade the wavefront perfection. A simple method was to insert in front of the collimating lens the polycarbonate plastic lid of a CD box. These are visibly of poor optical quality and in conjunction with the collimator represented an optical component that would normally be rejected.

Using the identical mirror and specimen, but passing the illuminating beam through the lid the integrated aberrations introduced several wavelengths of error, equivalent to a strain on the specimen which exceeded 0.02%. The resultant interference fringe pattern is shown in fig. 8.

With the plastic lid still in position, applying DMS and introducing a simulated uniform load, a figure similar to Figure 2(b) resulted. The uniformity of spacing and straightness of the fringes indicated again that the interferometer was well corrected and the uncertainty of measurement, of the order of  $\pm 0.1$

of a wavelength, was equivalent to a few microstrain -  
a virtually strain-free field.

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Preferred embodiments of the present invention

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are used in the mechanical behaviour measurement of  
5 components.

In testing components that are subject to high  
levels of strain, hundreds of interference fringes may  
be generated and whose orientations vary greatly. This  
will present problems in applying successfully  
10 automatic fringe analysis by the traditional approach.  
With DMS, the test interferogram of the high strain  
condition can be stored as a new reference, i.e. a  
"snapshot" of the interference fringe pattern can be  
taken at a particular moment in time, for use as a  
15 reference image. The interferometer is then reset to  
a null fringe condition, so that subsequent changes in  
the level of strain will appear as individual moiré  
fringes, rather than a subtle variation to a complex  
pattern. This process has important implications in  
20 the enhanced detection of special events in testing,  
such as the initiation of cracking and the onset of  
plastic deformation.

Other features, such as displaying a whole-field  
strain distribution in real-time have been successfully  
25 tested. Figure 4, shows a DMS interferogram from  
grating interferometry applied to a notched specimen  
at a gross displacement state. An additional small  
deformation of distribution, of approximately 1 micron  
is revealed above a non-uniform deformation exceeding  
30 50 microns.

The digital moiré interferograms may be analysed  
by a process including phase stepping.

Depending on the algorithm used, temporal phase  
stepping methods for the automatic analysis of fringe  
35 patterns required the capture of three or more

interferograms in order to calculate the phase distribution across the image (see e.g. Creath. K, Phase measurement interferometry techniques, Progress in optics. ed. Wolf, E. Chapter 5, Elsivier Sceience, B.V. (1988)). The process is usually performed on the test interferogram which has to be phase stepped by incrementally changing the path length in one arm of the interferometer. During stepping, it is usual to hold the component in a fixed condition.

5  
10 Applying the process to the analysis of DMS images, the phase stepping process needs to be carried out only on the initial reference image. The resulting stepped interferograms are then subtracted in turn from a single test interferogram, yielding a set of  
15 optically corrected images from which the phase distribution can be computed. This useful feature of a single test image offers the opportunity of conducting measurement under dynamic conditions. In addition, by recording a complete test program on  
20 videotape, or by other means it is practical for the operator to choose a particular image for detailed analysis by this method.

Embodiments of the present invention also find application in large aperture interferometry.

25 Apart from the facility for ameliorting the effects of gross aberrations of the optical components, another advantageous feature of digital moiré subtracting is its potential in large aperture interferometry. In a preliminary study, an  
30 interferometer based on the Fizeau design was constructed from simple components.

Figure 5, indicates that two nominally flat and parallel glass sheets (P1, P2) and a collimating lens can be used to demonstrate the principle of the  
35 approach. Interference takes place between the

wavefronts reflected from the rear surface of P1 and the front surface of P2. The combined wavefronts are re-focussed by the collimating lens and directed

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5       towards the CCD camera 2 via the beam-splitting glass plate P3. All the components are uncoated; hence the intensity of the emergent captured light is low, restricted by the combined reflections of approximately 4% at each interface of P1, P2 and P3. In addition, the contrast of the interferograms and  
10       the subsequent moiré image were reduced because of the limited coherence length of the HE-Ne laser and the dissimilar optical paths. A gap of approximately 100mm between P1 and P2 caused a marginal degradation of fringe contrast.

15       The dimensions of the collimating lens define the optical aperture of the interferometer. Trials with a 160 mm diameter plano-convex singlet lens, with a focal length of 750mm indicated that the initial fringe pattern showed of the order of 100 highly  
20       distorted fringes resulting from the unflatness of the plates and the spherical aberration in the lens. Consequently, there was no need to introduce additional tilt fringes before applying moiré subtraction. Results on introducing tilts to P2 as  
25       well as monitoring butane gas flow were similar to those shown in Figures 3(a) and (b) and extended to almost the whole 200mm aperture.

      A plastic Fresnel lens, removed from an overhead projector, was used as an alternative collimating  
30       lens. These are injection moulded and not intended for imaging purposes, but as light gatherers over extreme optical apertures. The lens examined consisted of two inwardly facing Fresnel lenses 280mm square and having an effective focal length of approximately 200mm  
35       ( $f/0.7$ ). It was not possible to image the

interferogram because of the large field angle. The double lens was separated and one was mounted, lens side inwards on a glass plate using silicone rubber.

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5 By filling the gap with water, the effective focal length was increased to approximately 800mm.

Provisional results showed that the imaging was not symmetric and poorly resolved, but acceptable fringe contrast and definition was achieved over an aperture of 220mm diameter (Figure 6). Although  
10 visible in the image, the circular structure of the Fresnel lens was not seriously conspicuous.

The trials indicate that it is feasible to use a Fresnel lens in embodiments of the present invention, but only where poor image quality can be tolerated.

15 In conclusion digital moiré subtraction allows the accurate measurement of a variety of optical components, mechanical and thermal behaviour and other parameters using optical interferometers which possess inherently poor optical quality. The method also  
20 offers the possibility of constructing very large aperture interferometers from inexpensive and imperfect optical components.

Each feature described in this specification (including the claims) may be incorporated in the  
25 present invention independently of other described features.

CLAIMS

- 
1. A measurement method comprising the steps of:
- 5     arranging an interferometer to form a first interference fringe pattern comprising at least ten interference fringes;
- recording an image of said first interference fringe pattern;
- 10    perturbing an optical path in the interferometer to form a second interference fringe pattern comprising at least ten interference fringes; and
- combining an image of said second interference fringe pattern with the recorded image of the first interference fringe pattern to produce a further image
- 15    comprising a moiré fringe pattern arising from a difference or differences between the first and second interference fringe patterns.
2. A measurement method in accordance with claim 1
- 20    wherein said arranging step includes the step of tilting a reflecting surface of the interferometer to increase the number of interference fringes in the first interference fringe pattern.
- 25    3. A measurement method in accordance with claim 1 or claim 2 wherein said first interference pattern comprises at least fifty interference fringes.
- 30    4. A measurement method in accordance with any preceding claim wherein said second interference fringe pattern comprises a larger number of interference fringes than the first interference fringe pattern.
- 35    5. A measurement method in accordance with any

preceding claim, wherein the step of perturbing includes the step of inserting a transparent object in the optical path.

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- 5        6.    A measurement method in accordance with any preceding claim, wherein the step of perturbing includes at least one of the steps of distorting, rotating and translating a reflecting surface in the optical path.
- 10
7.    A measurement method in accordance with any preceding claim, wherein the step of perturbing includes at least one of the steps of distorting, rotating and translating a transparent object in the optical path.
- 15
8.    A measurement method in accordance with any preceding claim wherein the step of perturbing includes the step of replacing a reference object with a test object.
- 20
9.    A measurement method in accordance with any preceding claim wherein the step of perturbing includes at least one of the steps of disturbing a gas, and disturbing a gas flow in the optical path.
- 25
10.   A measurement method in accordance with any preceding claim, wherein said image of the second interference fringe pattern is a recorded image.
- 30
11.   A measurement method in accordance with any preceding claim wherein at least one of the recorded image of the first interference fringe pattern and the image of the second interference pattern is an image selected from a recorded sequence of images of the
- 35

interference fringe pattern formed by the interferometer.

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5 12. A measurement method in accordance with any preceding claim, wherein the recorded image of the first interference fringe pattern and the image of the second interference fringe pattern are digital images.

10 13. A measurement method in accordance with claim 12 wherein the step of combining includes the step of subtracting one of the digital images from the other.

15 14. A measurement method in accordance with claim 13, wherein the step of combining includes the step of converting negative values obtained in the subtracting step to positive values.

20 15. A measurement method in accordance with any one of claims 12 to 14, wherein the digital images are images captured by a CCD camera.

25 16. A measurement method in accordance with any preceding claim, further comprising the steps of:  
arranging the interferometer to form a third interference fringe pattern;  
recording an image of the third interference fringe pattern;  
arranging the interferometer to form a fourth interference fringe pattern;  
30 recording an image of the fourth interference fringe pattern, wherein the first, third and fourth interference fringe patterns are phase shifted from each other by predetermined amounts; and  
combining the image of the second interference  
35 fringe pattern with each of the recorded images of the



first, third and fourth interference fringe patterns to produce respective said further images; and processing the further images to produce a phase map of the perturbation of the optical path.

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5

17. A measurement method in accordance with claim 16 wherein said images of the third and fourth interference fringe patterns are digital images.

10

18. A measurement method comprising the steps of:  
arranging an interferometer to form an interference fringe pattern comprising at least ten interference fringes;

15

recording an image of the interference fringe pattern at a selected time;

perturbing an optical path in the interferometer to alter the interference fringe pattern;

20

combining the recorded image with each one of a sequence of images of the interference fringe pattern at respective different times to produce a sequence of respective further images each comprising a moiré fringe pattern arising from a difference between the recorded image and the respective one of the sequence of images.

25

19. A measurement method in accordance with claim 18 wherein the recorded image and the sequential images are digital images.

30

20. A measurement method in accordance with claim 19 wherein the step of combining includes the step of subtracting one digital image from another.

35

21. A measurement method in accordance with claim 20, further comprising the step of displaying the sequence

of respective further images.

---

22. A measurement method in accordance with claim 21,

5 wherein the sequence of images of the interference  
fringe pattern is captured by a camera at a rate, and  
the sequence of respective further images is displayed  
at or substantially at said rate.

23. Measurement apparatus comprising:

10 an interferometer arranged to form interference  
fringe patterns comprising at least ten interference  
fringes;

a camera arranged to capture images of the  
interference fringe patterns;

15 an image store arranged to store an image of the  
interference fringe pattern captured by the camera at  
a selected time;

an image processor arranged to combine the stored  
image with an image of the interference fringe pattern  
20 captured by the camera at a different time to produce  
a further image comprising a moiré fringe pattern  
arising from a difference or differences between the  
interference fringe patterns at the selected and said  
different time.

25

24. Measurement apparatus in accordance with claim 23  
wherein the interferometer is arranged to form  
interference fringe patterns comprising at least fifty  
interference fringes.

30

25. Measurement apparatus in accordance with any one  
of claims 23 or 24, wherein said images are digital  
images.

35

26. Measurement apparatus in accordance with claim

25, wherein the image processor is arranged to produce the further image by a process including at least the subtraction of one of the digital images from the other.

---

5

27. Measurement apparatus in accordance with claim 26 wherein the image processor is arranged to produce the further image by a process including the conversion of negative values obtained in the subtraction to positive values.

10

28. Measurement apparatus in accordance with any one of claims 23 to 27, wherein the interferometer includes means for phase shifting the interference fringe patterns by predetermined amounts,

15

the image store is arranged to store images of the interference fringe patterns captured by the camera at at least three different selected times,

the image processor is arranged to combine each stored image with said image captured at a different time to produce a respective further image comprising a respective moiré fringe pattern, and

20

the image processor is further arranged to process the further images to produce a phase map.

25

29. Measurement apparatus in accordance with any one of claims 23 to 28 wherein the camera is arranged to output a sequence of said captured images,

the image processor is arranged to combine the or one of the stored images with each one of the sequence of captured images in turn to produce a respective said further image,

30

the apparatus further comprising at least one of: a display for displaying the sequence of further images; and

35

means for storing the sequence of further images.

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30. Measurement apparatus in accordance with claim

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29, wherein the camera is arranged to output the  
5 sequence of captured images at a rate, and the  
apparatus is further arranged to display the sequence  
of further images at said rate.

31. Measurement apparatus in accordance with any one  
10 of claims 23 to 29, further comprising an image  
recorder for recording the images captured by the  
camera, and an image selector for selecting one of the  
recorded images as an image to be stored in the image  
store or an image to be combined with a stored image.

15 32. Measurement apparatus in accordance with any one  
of claims 23 to 31 wherein the camera is a CCD camera.

20 33. Measurement apparatus in accordance with any one  
of claims 23 to 32, wherein the interferometer has an  
aperture of at least 10 cm.

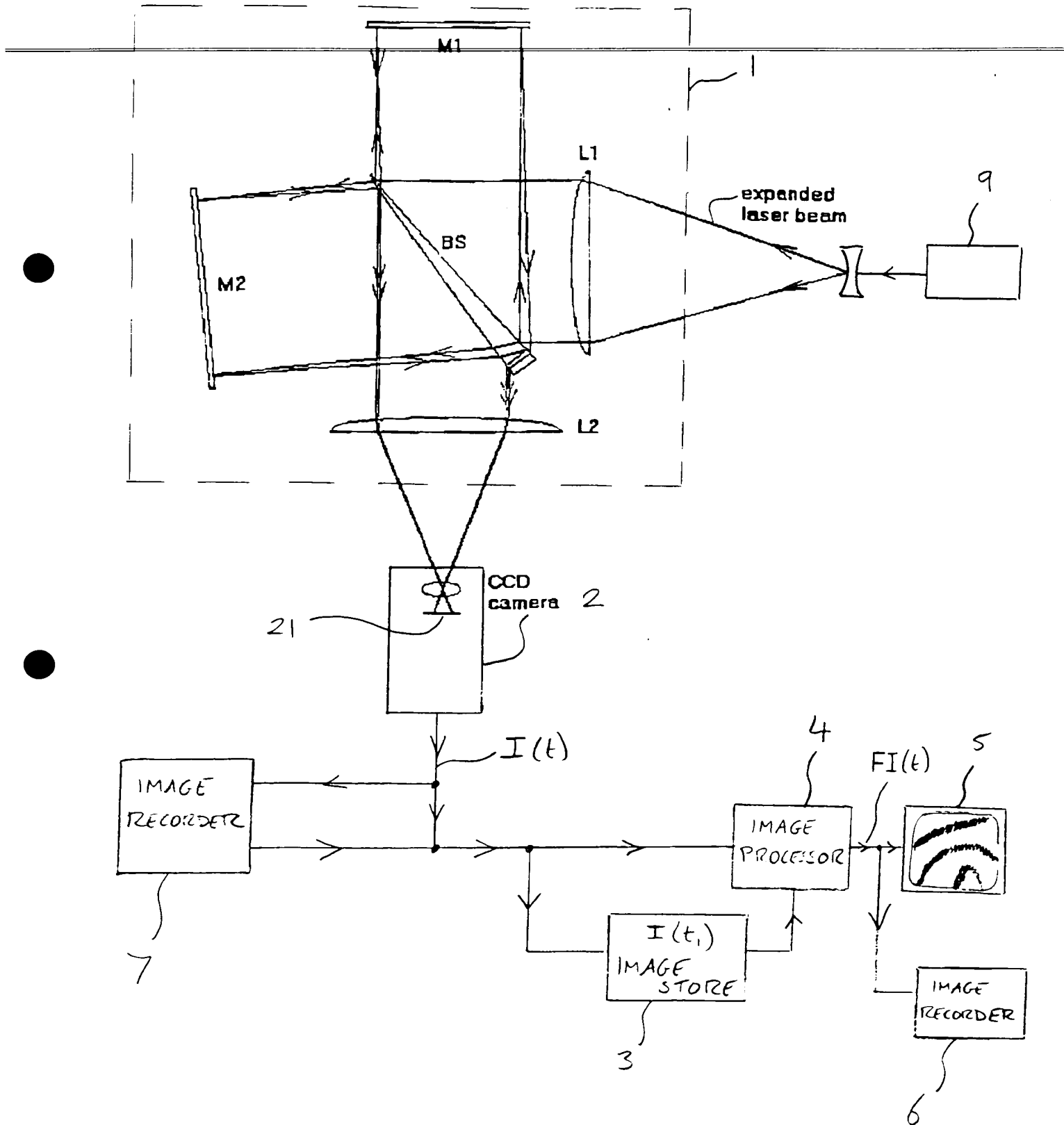
25 34. A measurement method substantially as  
hereinbefore described with reference to the  
accompanying drawings.

35. Measurement apparatus \_\_\_\_\_  
substantially as hereinbefore described with reference  
to the accompanying drawings.

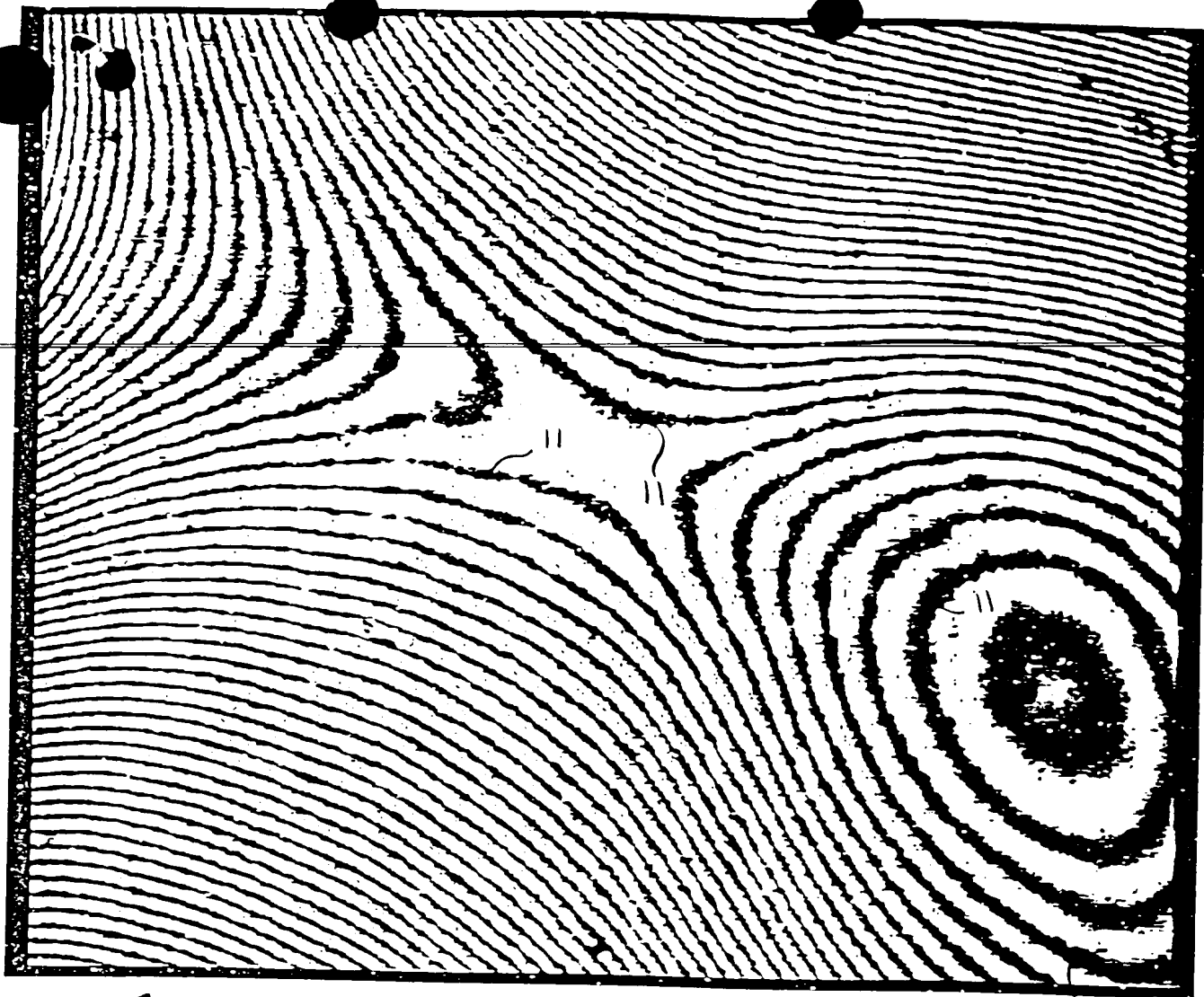
30

1/10

Fig. 1







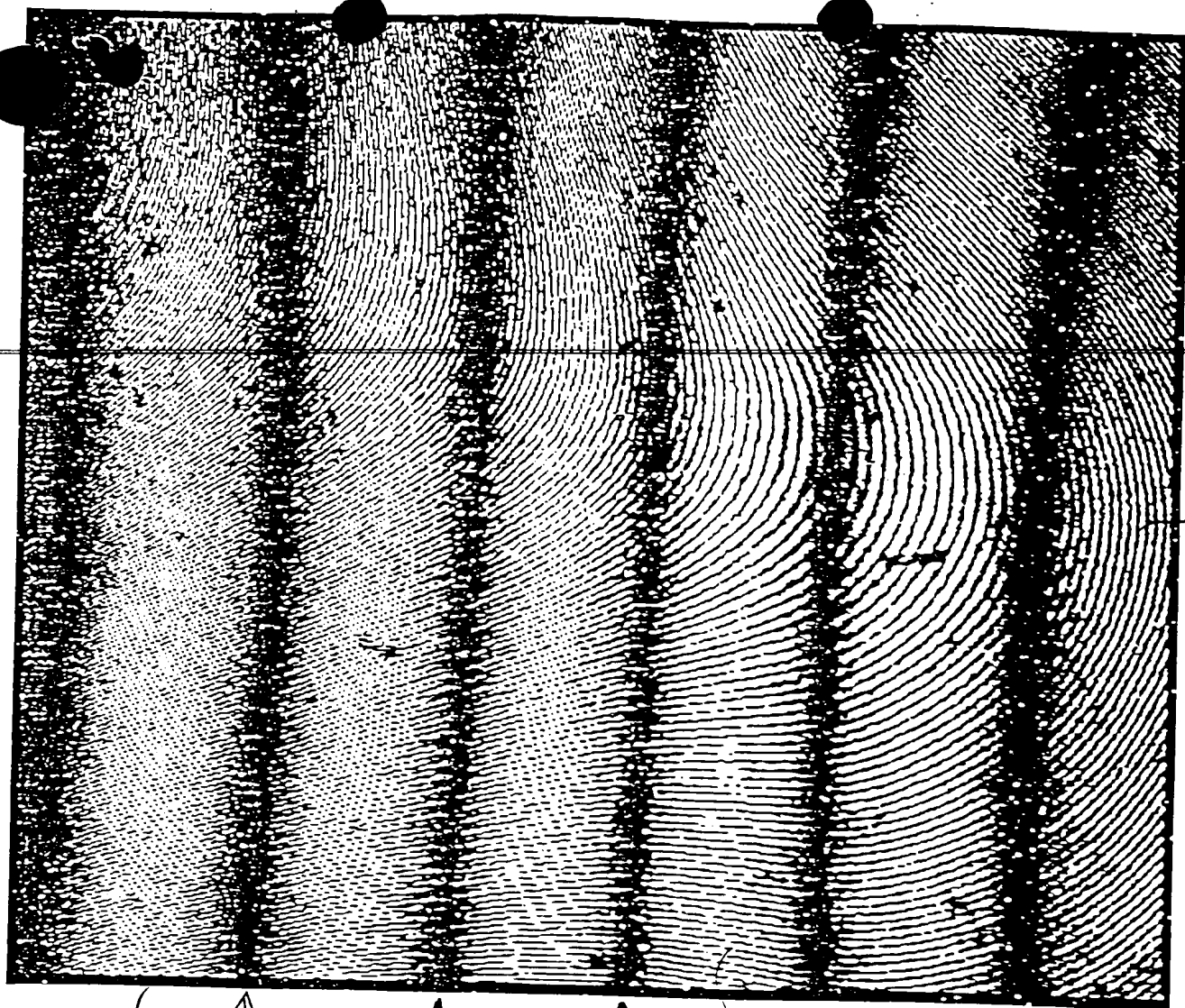
$I(t)$

Fig 2(a)

"





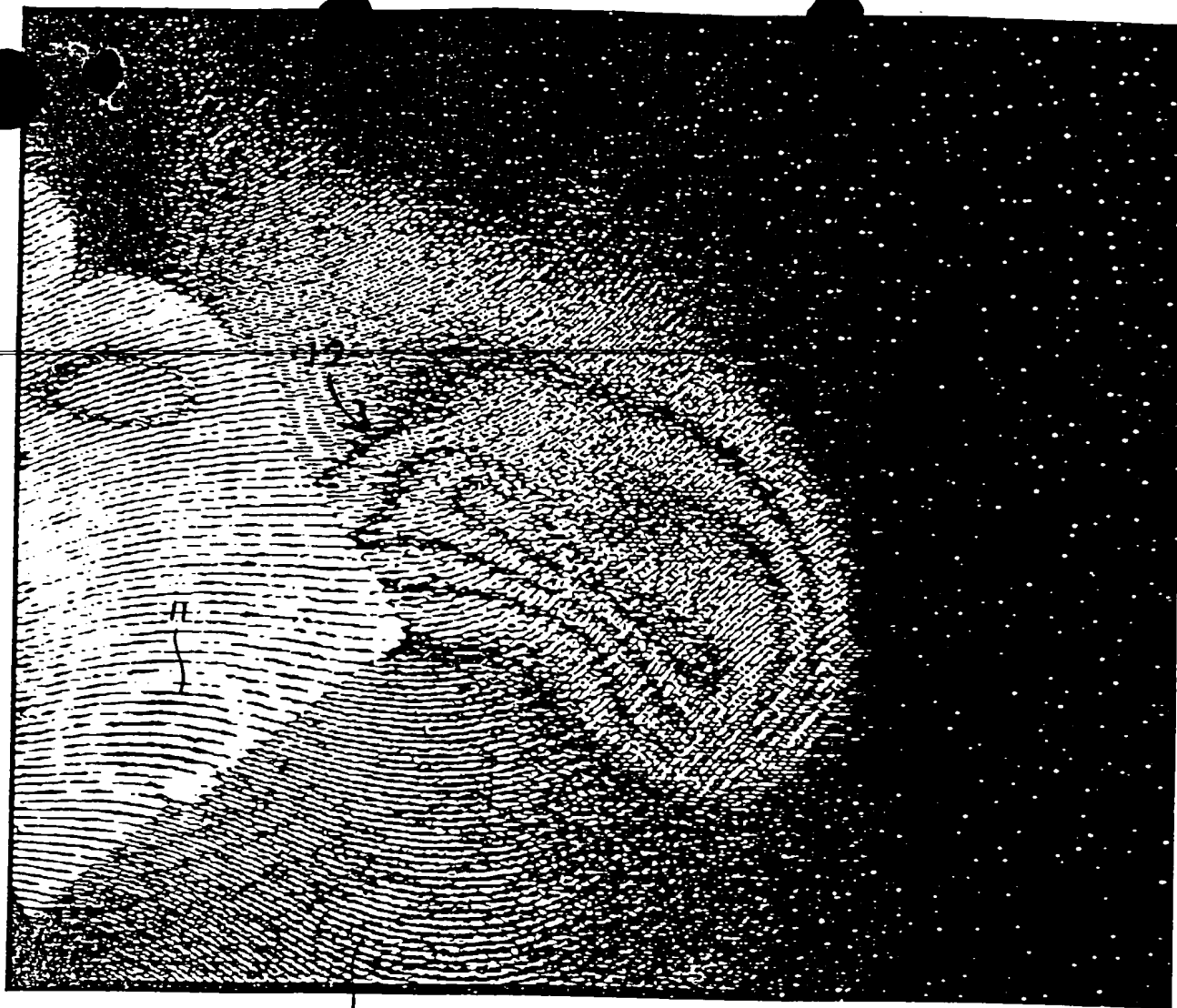


FI  
12  
12  
12  
12  
12

Fig 2(b)

FI





11

FI

Fig. 3(a)



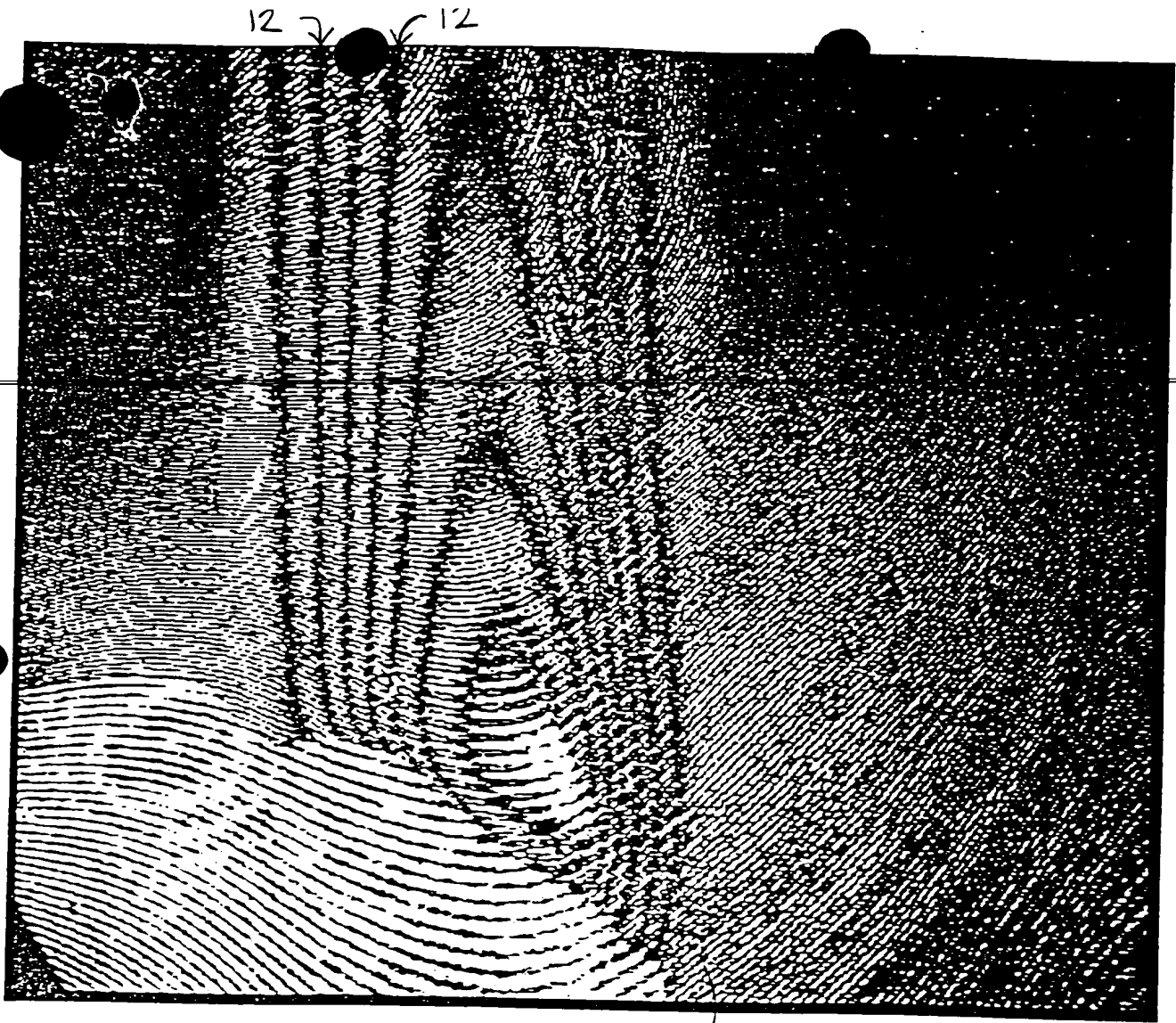


Fig. 3(b)



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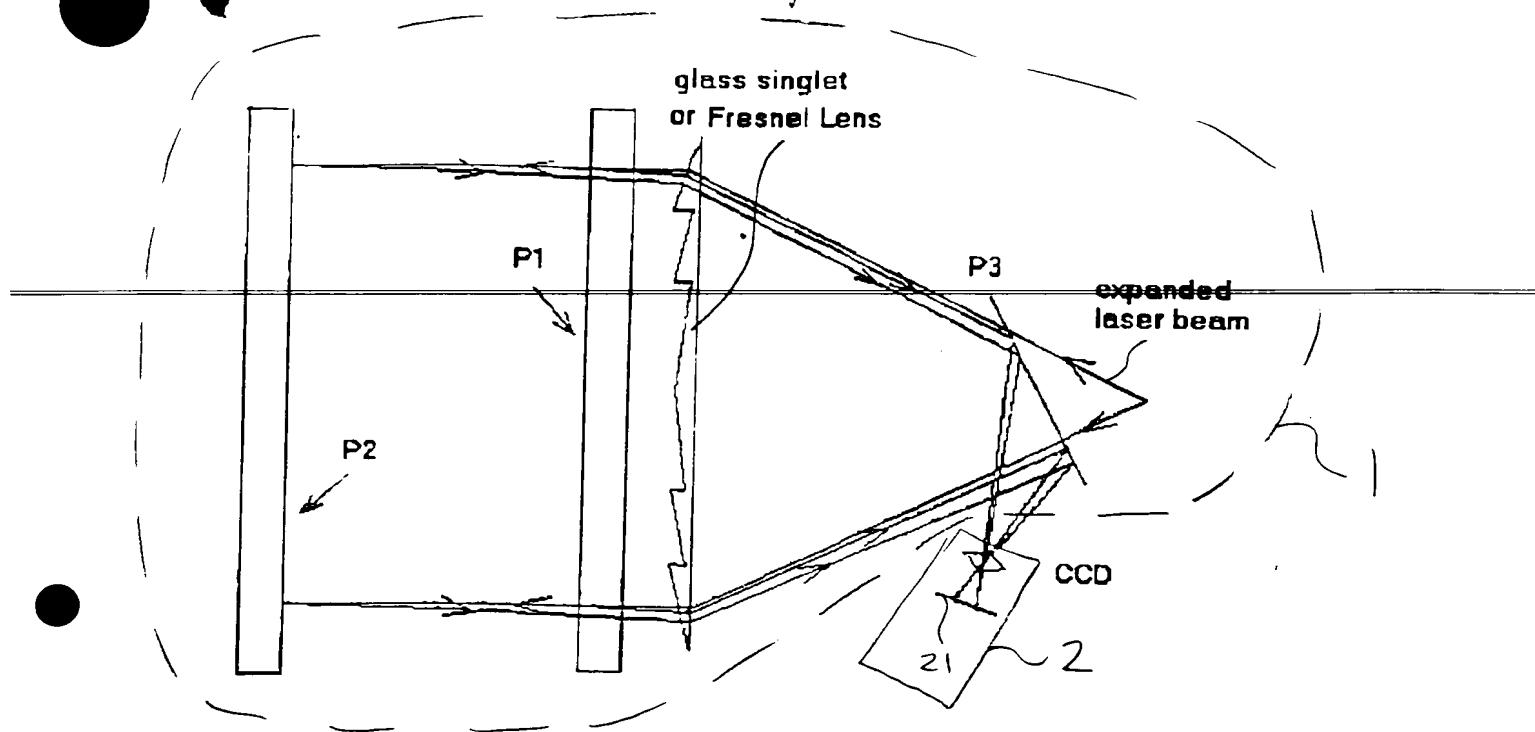


Fig. 5

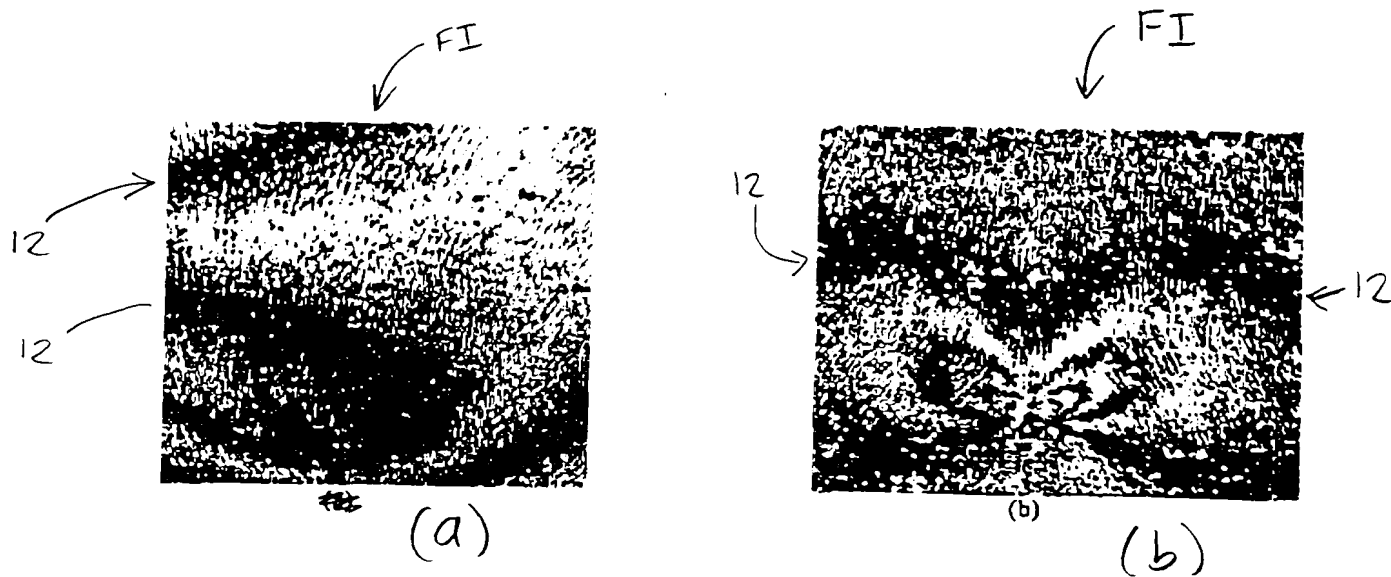
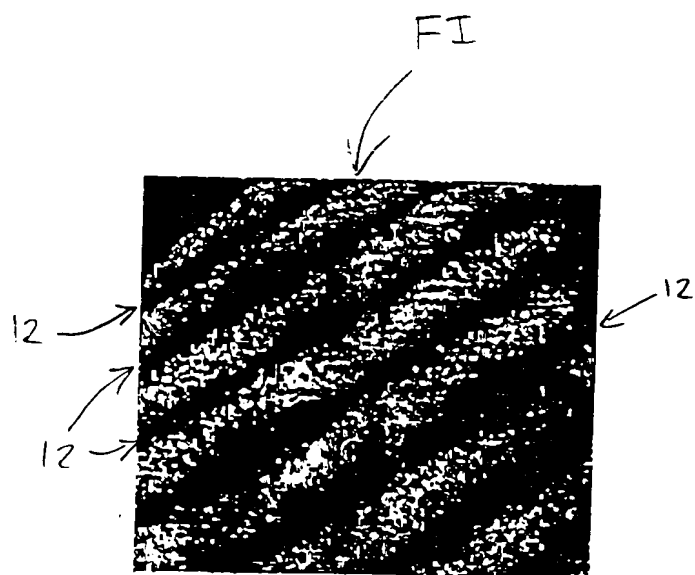


Fig 4

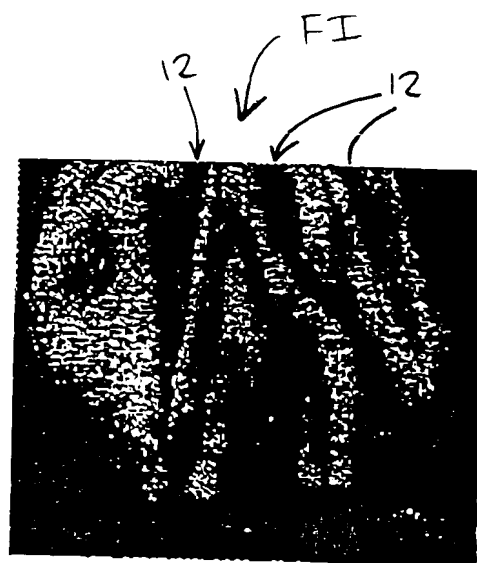




7/10



(a)



(b)

Fig 6



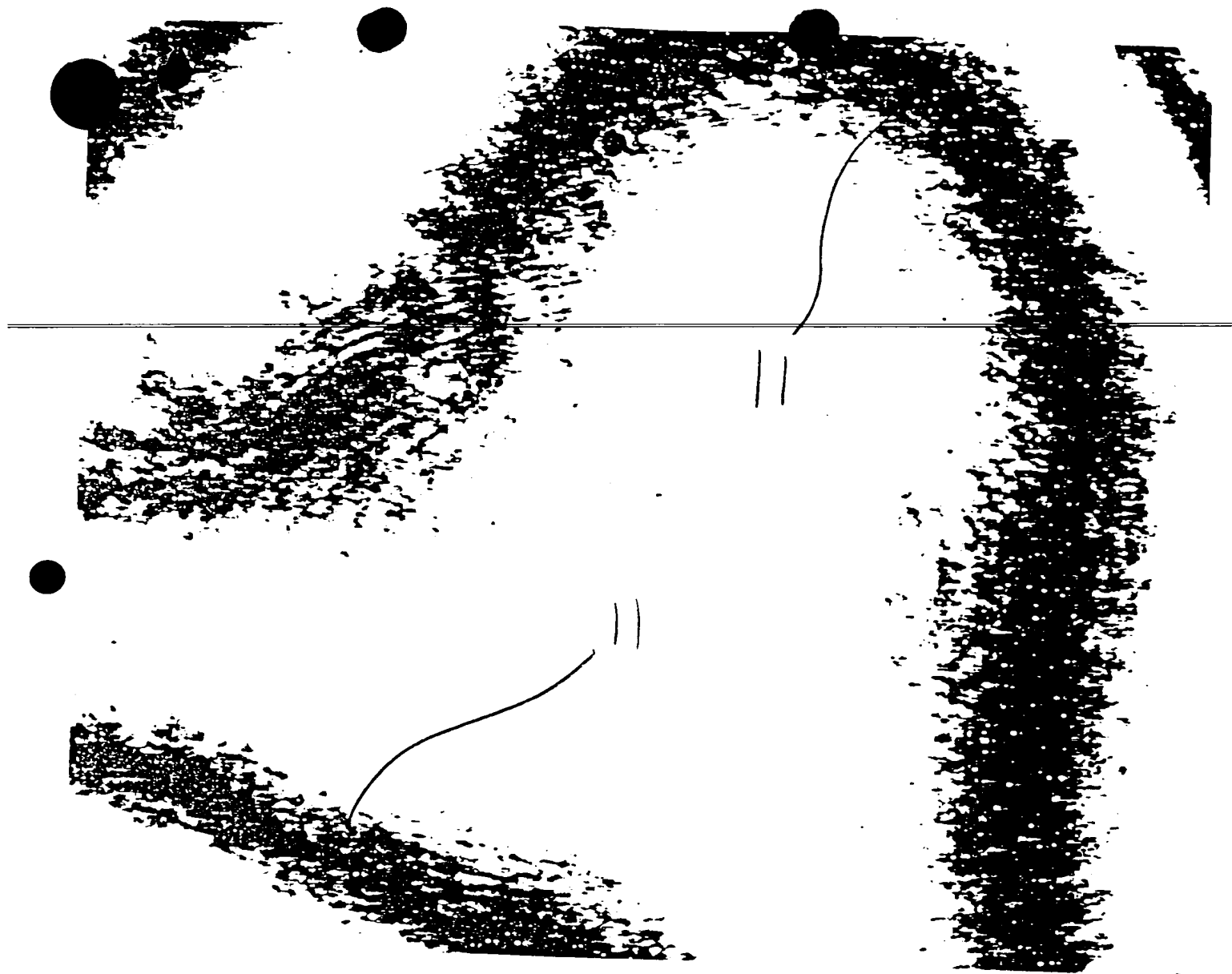


Fig. 7

8/10



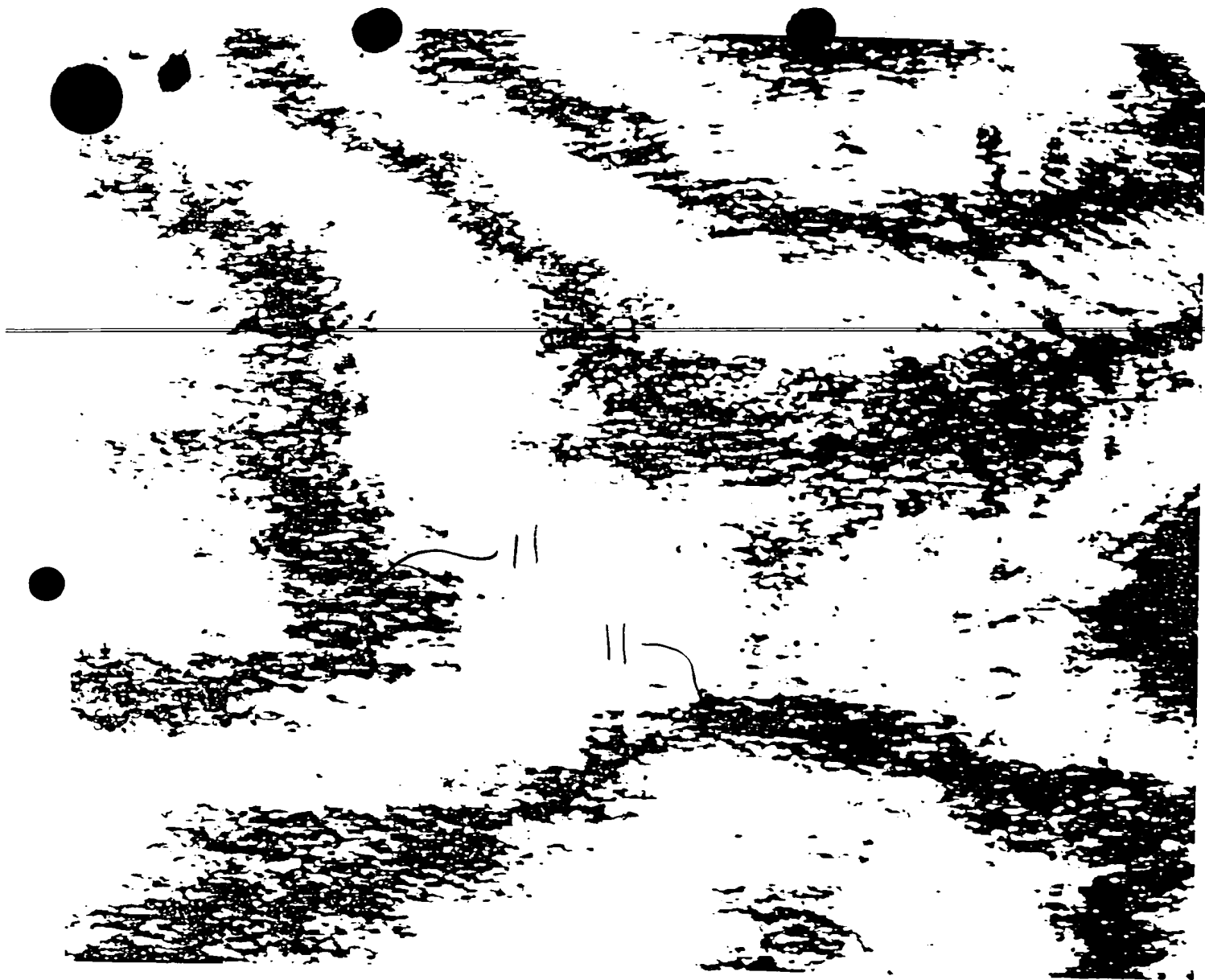


Fig. 8



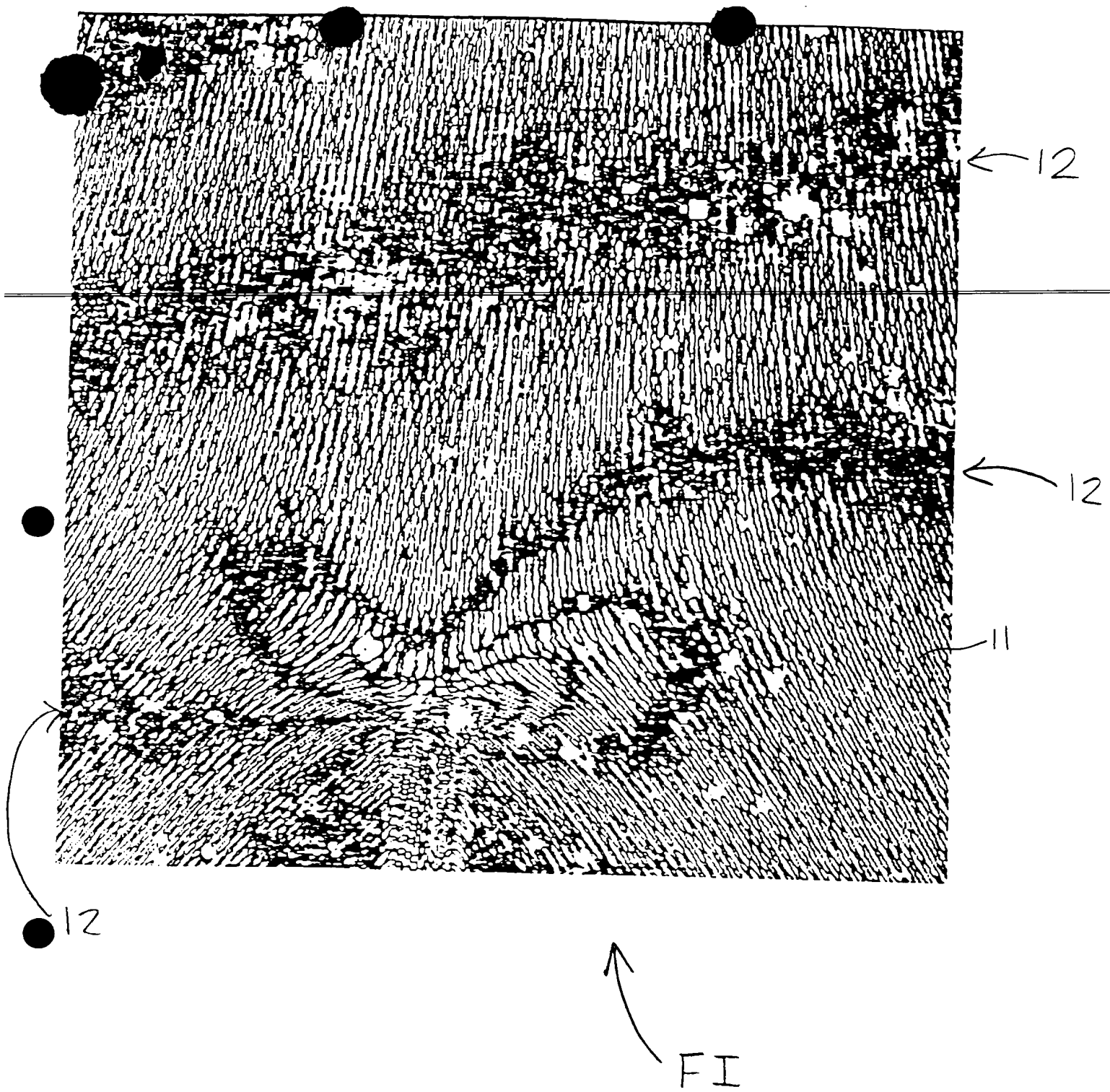


Fig 9







Application No: GB 9903638.6  
Claims searched: 1 to 35

Examiner: Julyan Elbro  
Date of search: 10 May 1999

**Patents Act 1977**  
**Search Report under Section 17**

**Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK Cl (Ed.Q): G1A (ACA, ACEF, ACEx); G2J (J7X)

Int Cl (Ed.6): G01B 9/02, 11/16, 11/24, 11/30; G01D 5/38; G01J 9/02

Other: ONLINE: EPODOC JAPIO WPI

**Documents considered to be relevant:**

Category	Identity of document and relevant passage	Relevant to claims
A	US 4981360 SCHWARZ	

X Document indicating lack of novelty or inventive step  
Y Document indicating lack of inventive step if combined with one or more other documents of same category.  
& Member of the same patent family

A Document indicating technological background and/or state of the art.  
P Document published on or after the declared priority date but before the filing date of this invention.  
E Patent document published on or after, but with priority date earlier than, the filing date of this application.

